

# Lecture 6: Experiment 5

## EE380 (Control Systems)

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# Announcements

- Before doing an experiment, download latest versions of supporting documents from Brihaspati.
- Latest version of program listings are on Brihaspati.
- Turn off power supply to board when not programming dsPIC or taking readings.
- After completion of experiment
  - Shut down PC, FG, PS.
  - Remove PICkit 2 from dsPIC board.



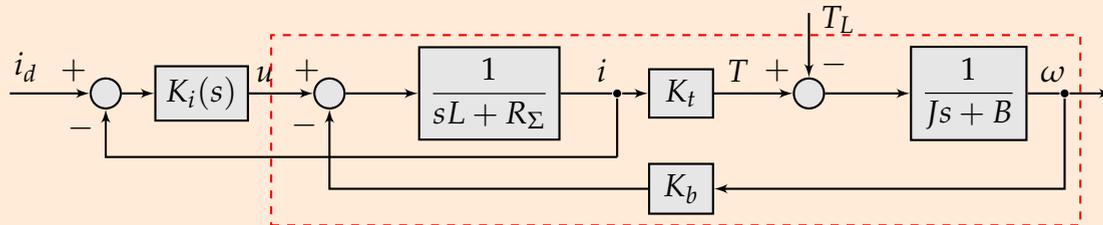
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# Outline of the experiment

- Design  $K_i(s)$  such that  $i$  tracks  $i_d$ .



Plant: The part outside dsPIC30F4012

- Use  $\hat{i} \approx i_{\text{sens}}/1.8 - 1/30$ . Is this a good approximation?
- Determine a trackable  $i_d$  using

$$\text{fundamental torque equation } J \frac{d\omega}{dt} = -B\omega + T - T_L$$

$$\text{voltage equation } V = L \frac{di}{dt} + Ri + E$$



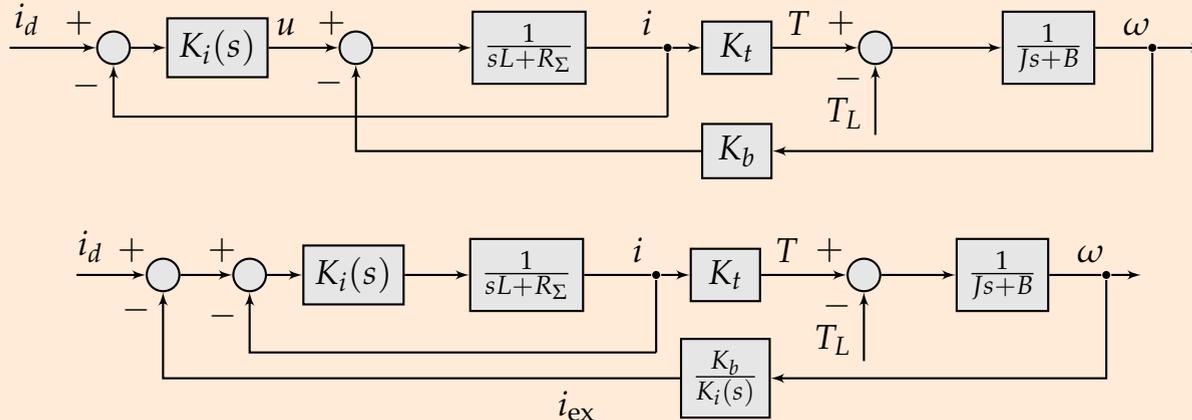
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# How to design a $K_i(s)$ ?

- Redraw block diagram



- $i$  tracks  $i_d - i_{ex}$ , not  $i_d$  alone.  $i$  is called well-regulated if it tracks  $i_d$  nicely. Nice tracking won't happen while  $i_{ex}$  dominates.  $\therefore$  choose  $K_i(s)$  to suppress  $i_{ex}$ . Two choices for  $K_i(s)$  are P and PI.
- P gives same gain in transient and SS  $\Rightarrow$  large demand on  $u$ . PI places small demand on  $u$  in transient and acceptable demand in SS. Also,  $\exists$  current filter to reject noise in  $i_{sens}$ .  $\Rightarrow$  Choose PI.



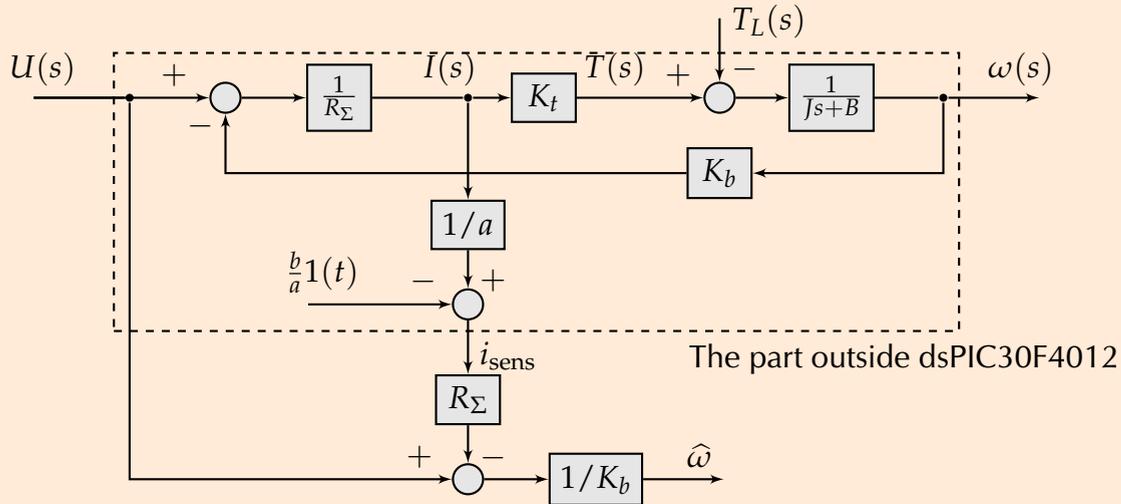
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# Is $\hat{i} \approx \frac{i_{\text{sens}}}{1.8} - \frac{1}{30}$ a good approximation?

- From Exp-t 4 saw that don't have an accurate relationship  $i = f(i_{\text{sens}})$ .
- Need to review the derivation that leads to  $\begin{bmatrix} b \\ a \end{bmatrix} = \begin{bmatrix} R_{\Sigma} & 7 - K_b \hat{\omega}_{ss7} \\ R_{\Sigma} & 9 - K_b \hat{\omega}_{ss9} \end{bmatrix}^{-1} \begin{bmatrix} 7 \\ 9 \end{bmatrix} \times \alpha$



- With an accurate relationship  $i = f(i_{\text{sens}})$  can have  $\omega \approx \hat{\omega}$  in Exp-t 4.
- For now, let us live with  $\hat{i} \approx \frac{i_{\text{sens}}}{1.8} - \frac{1}{30}$  or whatever gave you  $\omega$  closest to  $\hat{\omega}$  in Exp-t 4. Consequences to be seen in experiment on DOB.

## What is a trackable $i_d$ ?

We define a trackable  $i_d$  as one that does not need  $u$  to go into saturation. In our case  $u$  saturates at about 9 – 10 V. So, let us find  $i_d$  that needs  $u \leq 9$  V for the applied  $T_L$ .

- $L \approx 0$  (see, e.g., Exp-t 4)  $\Rightarrow u = R_\Sigma i + E \Rightarrow \boxed{u = R_\Sigma i + K_b \omega}$ .
- At  $\omega_{ss}$ ,  $\dot{\omega} = 0 \Rightarrow T = K_t i = T_L + B\omega \Rightarrow \boxed{\omega = \frac{K_t i - T_L}{B}}$ .
- From the two boxed equations, write an equation in terms of  $u, i, T_L$  by eliminating  $\omega$ :

$$u + \frac{K_b}{B} T_L = \left( R_\Sigma + \frac{K_b K_t}{B} \right) i$$

- For  $u = 9$  V,  $T_L = 0$ , find  $i_{d1}$ . For  $u = 9$  V,  $T_L = 0.003$  Nm, find  $i_{d2}$ . These are max. trackable currents.
- The min. trackable currents are obtained from  $i = T_L / K_t$ .



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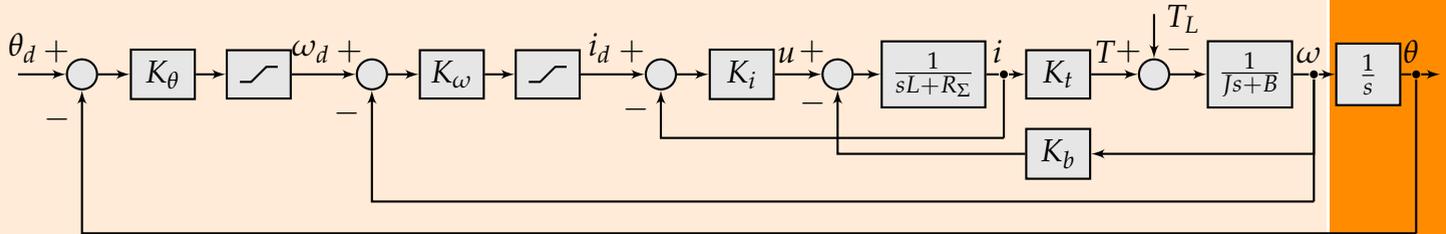
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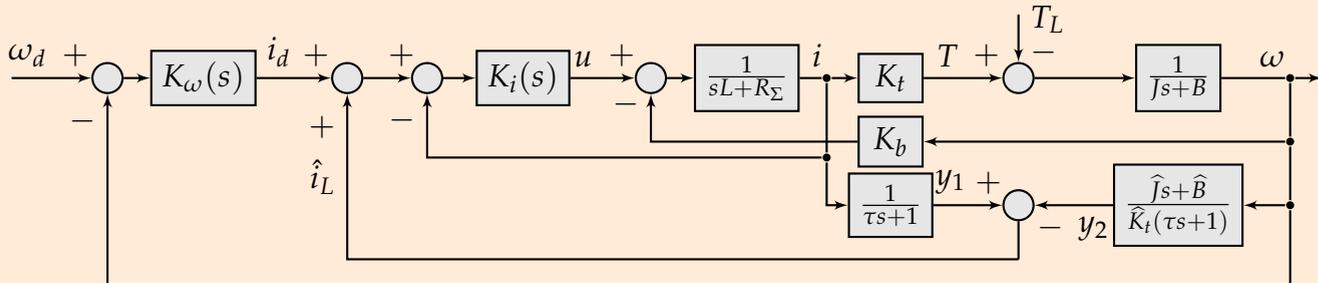
# Where is $i$ tracking $i_d$ useful?

Abbreviation:  $K_\theta \equiv K_\theta(s)$ ,  $K_\omega \equiv K_\omega(s)$ ,  $K_i \equiv K_i(s)$ .

Position control of pmdc motor while restricting speed and current.



Disturbance observer (DOB): Exp-t 6.



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# Homework (HW) vs. Lab work (LW)

HW

Determine TF from  $u$  to  $i$  for our pm dc motor module. Use  $R_\Sigma$  &  $B$  found experimentally.

Choose PI controller for  $t_s = 0.5$  s

Determine max. values of  $i_{d1}$  &  $i_{d2}$

Simulate CL sys using modified `easysim.m` for  $i_{d1}$  &  $i_{d2}$

Plot  $i_1$  vs.  $t$  &  $i_2$  vs.  $t$  on one figure.  
Plot  $u_1$  vs.  $t$  &  $u_2$  vs.  $t$  on one figure.

LW

In `main-prog.c`: code PI controller; implement control of  $i$ ; use  $i = f(i_{sens})$  that gave best results in Exp-t 4.

Track  $90\%i_{d1}$  and  $90\%i_{d2}$ .  $i_{d2}$  provided by 1.5 kg weight hanging from pulley.

While pulley rotating, in both cases stall and release pulley

Take plots in both cases before and after application of additional  $T_L$

Comment on dist. rej. & tracking.



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# Discretization

$$\frac{a_1 s + a_0}{s^2 + b_1 s + b_0}$$

Simulation  
diagram

$$\begin{aligned}\dot{x}_1 &= x_2 \\ \dot{x}_2 &= -b_0 x_1 - b_1 x_2 + u \\ y &= a_0 x_1 + a_1 x_2\end{aligned}$$

Euler's  
approximation

$$\begin{aligned}x_{1(k+1)} &= x_{1(k)} + \Delta t x_{2(k)} \\ x_{2(k+1)} &= -b_0 \Delta t x_{1(k)} + (1 - b_1 \Delta t) x_{2(k)} + \Delta t u_k \\ y_k &= a_0 x_{1(k)} + a_1 x_{2(k)}\end{aligned}$$



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# Simulate; LW: C code, Implement, Analyze

- Simulation: `easysim.m`
- Discretized controller  
→ C code:
- Implement: As in demo slides
- Analyze: Compare results

$$\begin{aligned}x_1(k+1) &= a_{11}x_1(k) + a_{12}x_2(k) + b_1u(k) \\x_2(k+1) &= a_{21}x_1(k) + a_{22}x_2(k) + b_2u(k) \\y(k) &= c_1x_1(k) + c_2x_2(k) + du(k)\end{aligned}$$

In `main-prog.c` before `main()` insert `float x1[2], x2[2];`  
In `main()` insert `x1[0] = x2[0] = 0;`

```
x1[1] = a11 * x1[0] + a12 * x2[0] + b1 * u;
x2[1] = a21 * x1[0] + a22 * x2[0] + b2 * u;
y = c1 * x1[0] + c2 * x2[0] + d * u;
x1[0] = x1[1];
x2[0] = x2[1];
```



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